

pas de pesanteur

$$\begin{aligned} \vec{OG}_2 &= \vec{OA} + \vec{AG}_2 = (a+x) \vec{i} + b (-\sin \alpha \vec{i} + \cos \alpha \vec{j}) \\ &= (a+x - b \sin \alpha) \vec{i} + b \cos \alpha \vec{j} \end{aligned}$$

$$\frac{d\vec{OG}_2}{dt} = (\dot{x} - b \cos \alpha \dot{\alpha}) \vec{i} - b \sin \alpha \dot{\alpha} \vec{j}$$

$$T = \frac{1}{2} m_1 \dot{x}^2 + \frac{1}{2} m_2 \left[ (\dot{x} - b \cos \alpha \dot{\alpha})^2 + (b \sin \alpha \dot{\alpha})^2 \right] + \frac{1}{2} J_2 \dot{\alpha}^2$$

$$\frac{\partial T}{\partial \dot{x}} = m_1 \dot{x} + m_2 \dot{x} - b \cos \alpha m_2 \dot{\alpha}$$

$$\frac{d}{dt} \frac{\partial T}{\partial \dot{x}} = (m_1 + m_2) \ddot{x} - b \cos \alpha m_2 \ddot{\alpha} + b \sin \alpha m_2 \dot{\alpha}^2$$

$$-\frac{\partial T}{\partial x} = 0$$

$$\frac{\partial T}{\partial \dot{\alpha}} = m_2 b^2 \dot{\alpha} - m_2 b \cos \alpha \dot{x} + J_2 \dot{\alpha}$$

$$\frac{d}{dt} \frac{\partial T}{\partial \dot{\alpha}} = (J_2 + m_2 b^2) \ddot{\alpha} - m_2 b \cos \alpha \ddot{x} + m_2 b \sin \alpha \dot{\alpha} \dot{x}$$

$$-\frac{\partial T}{\partial \alpha} = -m_2 b \sin \alpha \dot{\alpha} \dot{x}$$

$$V = \frac{1}{2} k_1 x^2 + \frac{1}{2} k_2 \alpha^2$$

$$-\frac{\partial V}{\partial x} = -k_1 x$$

$$-\frac{\partial V}{\partial \alpha} = -k_2 \alpha$$

$$\begin{bmatrix} -m_2 b \cos \alpha & J_2 + m_2 b^2 \end{bmatrix} \begin{bmatrix} \ddot{x} \\ \ddot{\alpha} \end{bmatrix} + \begin{bmatrix} k_1 & 0 \\ 0 & k_2 \end{bmatrix} \begin{bmatrix} x \\ \alpha \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} (m_1 + m_2) & -b m_2 \cos \alpha \\ -m_2 b \cos \alpha & J_2 + m_2 b^2 \end{bmatrix} \begin{bmatrix} \ddot{x} \\ \ddot{\alpha} \end{bmatrix} + \begin{bmatrix} b \sin \alpha m_2 \dot{\alpha}^2 \\ m_2 b \sin \alpha \dot{\alpha} \dot{x} \end{bmatrix} = \begin{bmatrix} -k_1 x \\ 0 - k_2 \alpha \end{bmatrix}$$

Pour  $\alpha, x$  ~~petits~~ petits  
 $\dot{\alpha}, \dot{x}$  petits

$$\begin{bmatrix} m_1 + m_2 & -b m_2 \\ -b m_2 & J_2 + m_2 b^2 \end{bmatrix} \begin{bmatrix} \ddot{x} \\ \ddot{\alpha} \end{bmatrix} + \begin{bmatrix} k_1 & 0 \\ 0 & k_2 \end{bmatrix} \begin{bmatrix} x \\ \alpha \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

Posons  $\tilde{m} = m_2/m_1$   $\tilde{J} = J_2$

$$y = b \alpha$$

$$\begin{bmatrix} m_1 (1 + \tilde{m}) & -m_1 \tilde{m} b \\ -m_1 \tilde{m} & \tilde{J}_2 + m_1 \tilde{m} b^2 \end{bmatrix}$$

Posons  $\tilde{x} = \frac{x}{b}$

$$\begin{bmatrix} b(m_1 + m_2) & -b^2 m_2 \\ -b^2 m_2 & J_2 + m_2 b^2 \end{bmatrix} \begin{bmatrix} \ddot{\tilde{x}} \\ \ddot{\alpha} \end{bmatrix} + \begin{bmatrix} b k_1 & 0 \\ 0 & k_2 \end{bmatrix} \begin{bmatrix} \tilde{x} \\ \alpha \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$J_2 = \tilde{J} (m_2 b^2)$$

$$\tilde{m} = m_1/m_2$$

$$\begin{bmatrix} b(m_1 + m_2) & -b m_2 \\ -1 & \tilde{J}_2 + 1 \end{bmatrix} \begin{bmatrix} \ddot{\tilde{x}} \\ \ddot{\alpha} \end{bmatrix} + \begin{bmatrix} b k_1 & 0 \\ 0 & \frac{k_2}{m_2 b^2} \end{bmatrix} \begin{bmatrix} \tilde{x} \\ \alpha \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} \tilde{m} + 1 & -1 \\ -1 & \tilde{J}_2 + 1 \end{bmatrix} \begin{bmatrix} \ddot{\tilde{x}} \\ \ddot{\alpha} \end{bmatrix} + \begin{bmatrix} \frac{k_1}{m_2} & 0 \\ 0 & \frac{k_2}{m_2 b^2} \end{bmatrix} \begin{bmatrix} \tilde{x} \\ \alpha \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\omega_0^2 = \frac{k_1}{m_2}$$

$$\tilde{k} = \frac{k_2}{b^2 k_1}$$

$$\frac{N}{\log m} \quad \frac{k_2}{b^2} = \tilde{k} k_1$$

$$\begin{bmatrix} \tilde{m} + 1 & -1 \\ -1 & \tilde{J}_2 + 1 \end{bmatrix} \begin{bmatrix} \ddot{\tilde{x}} \\ \ddot{\alpha} \end{bmatrix} + \begin{bmatrix} \omega_0^2 & 0 \\ 0 & \tilde{k} \omega_0^2 \end{bmatrix} \begin{bmatrix} \tilde{x} \\ \alpha \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

Détermination de la première fréquence propre.

On cherche  $\begin{bmatrix} \tilde{x} \\ \tilde{y} \\ \tilde{z} \\ \tilde{w} \end{bmatrix} = \begin{bmatrix} X \\ A \end{bmatrix} \sin \tilde{\omega} t$

$$\left| -\tilde{\omega}^2 \begin{bmatrix} \tilde{m}+1 & -1 \\ -1 & \tilde{J}+1 \end{bmatrix} + \begin{bmatrix} \omega_0^2 & 0 \\ 0 & k \omega_c^2 \end{bmatrix} \right| = 0$$

$$\left| \begin{array}{cc} -\tilde{\omega}^2(\tilde{m}+1) + \omega_0^2 & \tilde{\omega}^2 \\ \tilde{\omega}^2 & -\tilde{\omega}^2(\tilde{J}+1) + k \omega_c^2 \end{array} \right| = 0$$

$$\tilde{\omega}^4 [(\tilde{m}+1)(\tilde{J}+1)] + \tilde{\omega}^2 [-(\tilde{J}+1) - (\tilde{m}+1)] + k - 1 - \omega_0^2 \omega_c^2 = 0$$

$\Delta = b^2 - 4ac$

$\Rightarrow$

$$\tilde{\omega}^4 [\tilde{m}\tilde{J} + \tilde{m} + \tilde{J} + 1] + \tilde{\omega}^2 [-\tilde{J} - \tilde{m} - 2] + k - 1 = 0$$

$\Delta = b^2 - 4ac$

~~$= [-\tilde{J} - \tilde{m} - 2]^2 - 4[\tilde{m}\tilde{J} + \tilde{m} + \tilde{J} + 1][k - 1]$~~

~~$\tilde{\omega}_1 = \frac{-b \pm \sqrt{\Delta}}{2a}$~~

$$\left| \begin{array}{l} k = 2 \\ \tilde{m} = 1 \\ \tilde{J} = 1 \end{array} \right.$$

$$\left| \begin{array}{l} k = 2 \\ \tilde{m} = 1 \\ \tilde{J} = 2 \end{array} \right.$$

3  $\tilde{\omega}^4 + \tilde{\omega}^2 [-4] + 1 = 0$

5  $\tilde{\omega}^4 + \tilde{\omega}^2 (-5) + 1 = 0$

$\Delta = 16 - 4 \times 4$

$\Delta = 25 - 4 \times 5 \times 1$

$= 16 - 4 \times 3$

$= 5$

$= 4$

$\Delta = 2$

$$\left\{ \begin{array}{l} \tilde{\omega}_1 = \frac{5 - \sqrt{5}}{10} = \frac{5 - \sqrt{5}}{10} \approx 0,276 \\ \tilde{\omega}_2 = \frac{5 + \sqrt{5}}{10} = \frac{5 + \sqrt{5}}{10} \approx 0,724 \end{array} \right.$$

## Vektors propres

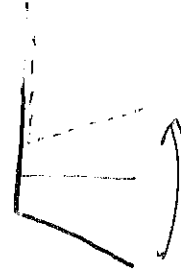
$$\bullet \bar{\omega}_1 \rightarrow \vec{v}_1 = \begin{bmatrix} x_1 \\ A_1 \end{bmatrix}$$

$$\left[ -\bar{\omega}_1^2 (\bar{m} + 1) + 1 \right] x_1 + \bar{\omega}_1^2 A_1 = 0$$

$$\left[ -\frac{10 + 2\sqrt{5}}{10} + 1 \right] x_1 + \frac{5 - \sqrt{5}}{10} A_1 = 0$$

$$A_1 = \frac{10}{5\sqrt{5}} \left[ -2 \frac{\sqrt{5}}{10} \right] x_1$$

$$A_1 = -\frac{2}{\sqrt{5}-1} x_1$$



$$\bullet \bar{\omega}_2 \rightarrow \vec{v}_2 = \begin{bmatrix} x_2 \\ A_2 \end{bmatrix}$$

$$\left[ -\bar{\omega}_2^2 (\bar{m} + 1) + 1 \right] x_2 + \bar{\omega}_2^2 A_2 = 0$$

$$\left[ -\frac{10 + 2\sqrt{5}}{10} + 1 \right] x_2 + \frac{5 + \sqrt{5}}{10} A_2 = 0$$

$$A_2 = +\frac{10}{5 + \sqrt{5}} \left[ +\frac{2\sqrt{5}}{10} \right] x_2$$

$$\boxed{A_2 = \frac{2}{\sqrt{5}+1} x_1}$$



Avec un oiseau en  $G_2$

l'inertie de rotation du solide  $\frac{2}{3}m$  est pas changée car l'oiseau reste vertical

la masse du solide 2 est modifiée par la masse de l'oiseau  $m_0$

$$m_2 \rightarrow m_2 + m_0$$

$$\text{si } m_0 = m_2 \rightarrow \tilde{m} : 1 \rightarrow \frac{1}{2}$$

$$\tilde{J} = 2$$

$$\tilde{k} = 2$$

$$\omega_0 \rightarrow \left[ \frac{\omega_0}{2} \right]$$

la pulsation propre <sup>adim.</sup> est donnée par.

$$\left[ \frac{1}{2} \cdot 2 + \frac{1}{2} + 2 \right] \tilde{\omega}^4 + \tilde{\omega}^2 \left[ -2 - \frac{1}{2} - 2 \right] + 1 = 0$$

$$\frac{7}{2} \tilde{\omega}^4 + \tilde{\omega}^2 \left( -\frac{9}{2} \right) + 1 = 0$$

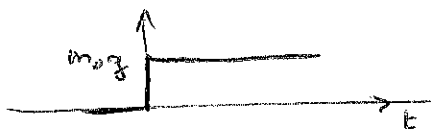
$$\begin{aligned} \Delta &= b^2 - 4ac \\ &= \frac{81}{4} - 4 \cdot \frac{7}{2} \\ &= \frac{81 - 56}{4} \\ &= \frac{25}{4} \end{aligned}$$

$$\sqrt{\Delta} = \frac{5}{2}$$

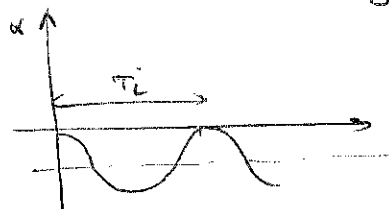
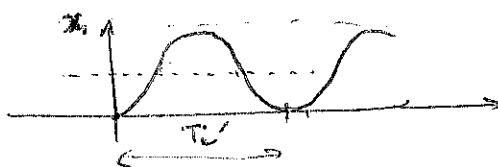
$$\left\{ \begin{aligned} \tilde{\omega}_1' &= \frac{\frac{9}{2} - \frac{5}{2}}{7} = \frac{4/2}{7} = \frac{2}{7} \approx 0,28 \\ \tilde{\omega}_2' &= \frac{\frac{9}{2} + \frac{5}{2}}{7} = 1 \end{aligned} \right.$$

$\omega_i = \tilde{\omega}_i \left( \frac{\omega_0}{2} \right) \rightarrow$  les pulsations baissent quasiment de moitié.

l'arrivée de l'oiseau peut être considérée comme un échelon de force sur le système avec une masse.

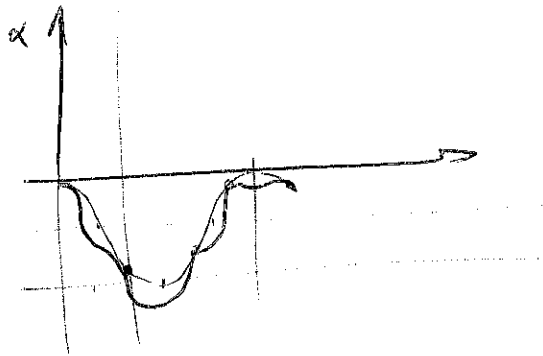
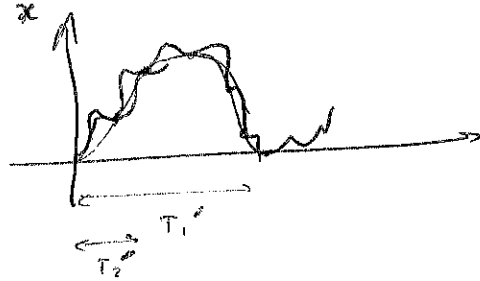


• ~~Sur~~ la réponse de chaque mode sera du type.



$$\text{avec } T_i' = \frac{2\pi}{\omega_i'}$$

d'où une réponse totale, superposition des deux réponses



la part de l'amplitude de chaque mode est calculable en décomposant la force sur les 2 vecteurs propres.

$$\begin{aligned}
 P &= \vec{F} \cdot \vec{V}_{b2} \\
 &= F H(t) \vec{e} \cdot \left[ (\ddot{x} - b \cos \alpha \dot{x}) \vec{e} + \ddot{y} \vec{j} \right] \\
 &= \underbrace{F H(t)}_{Q_2} \ddot{x} - \underbrace{b \cos \alpha F H(t)}_{Q_1} \dot{x}
 \end{aligned}$$

Les équations de mouvement ont donc comme second membre.

$$\begin{bmatrix} \text{---} \\ \text{---} \end{bmatrix} = \begin{bmatrix} F H(t) \\ -b F H(t) \end{bmatrix}$$

Pour connaître la part  $(q_1, q_2)$  de chaque mode  $\omega_1$  et  $\omega_2$  il suffit de décomposer le chargement dans la base modale.

$$\begin{bmatrix} F H(t) \\ -b F H(t) \end{bmatrix} = q_1 \begin{bmatrix} v_{11}^i \\ v_{12}^i \end{bmatrix} + q_2 \begin{bmatrix} v_{21}^i \\ v_{22}^i \end{bmatrix}$$